## Tutorial for MASTAN2 v5.1Pour Stop Beam




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## Credits

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## Section 1: Overview

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## Overview

This tutorial provides step-by-step guidance for the sample pour stop beam evaluation. Enough details are provided that the example model with non-doubly symmetric sections can be completed following the instructions here. Not every feature available in MASTAN2 will be mentioned nor utilized in this tutorial. For further information on many of the features within MASTAN2 make use of other tutorials at http://www.mastan2.com/tutorial.html.

## Problem Overview

This tutorial completes the analysis of a simply supported non-doubly symmetric section in MASTAN2 and some of the related stress calculations. The section considered is a pour stop that is simply supported. The values used in this tutorial come from the Steel Deck Institute's Technical Note

- No. 3: Pour Stops as Beams.


Simple Supported Beam


Cross Section

## Section 2: Getting Started



## MASTAN2 General Information

MASTAN2 is an interactive graphics program that provides preprocessing, analysis, and postprocessing capabilities. Preprocessing options include definition of structural geometry, support conditions, applied loads, and element properties. The analysis routines provide the user the opportunity to perform first- or second-order elastic or inelastic analyses of two- or three-dimensional frames and trusses subjected to static and dynamic loads. Postprocessing capabilities include the interpretation of structural behavior through deformation and force diagrams, printed output, and facilities for plotting response curves. MASTAN2 is based on MATLAB®, a premier software package for numeric computing and data analysis.

In many ways, MASTAN2 is similar to today's commercially available software in functionality. The number of pre- and post-processing options, however, have been limited in order to minimize the amount of time needed for a user to become proficient at its use. The program's linear and nonlinear analysis routines are based on the theoretical and numerical formulations presented in the text Matrix Structural Analysis, 2nd Edition, by McGuire, Gallagher, and Ziemian. In this regard, the reader is strongly encouraged to use this software as a tool for demonstration, reviewing examples, solving problems, and perhaps performing analysis and design studies. Where MASTAN2 has been written in modular format, the reader is also provided the opportunity to develop and implement additional or alternative analysis routines directly within the program.

MATLAB is a registered trademark of The MathWorks, Inc., 3 Apple Hill Drive, Natick, MA 01760-2098.

## Launching MASTAN2

Two versions of MASTAN2 have been developed and may be installed. One requires you to have access to MATLAB and the other does not. Both versions provide the same functionality, except that the MATLAB version also provides the user an opportunity to develop and implement additional or alternative analysis routines that will directly interact with MASTAN2. Please see the Setup Guides at www.mastan2.com.


## Base Layout

In order to minimize the learning time for MASTAN2, its graphical user interface (GUI) has been designed using a simple and consistent two menu approach. Using a pull-down menu at the top of the GUI, a command is selected. Parameters are then defined in the bottom menu bar and the command is executed by using the Apply button.


## Section 3: Beam Modeling

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## Problem Description - Figure

The pour stop is a cold-form steel cross-section. The section is subjected to a uniform lateral and uniform vertical load as well as a distributed torsion. The model itself will be a simply supported beam with the ends fixed for torsion, but free to warp. Details on the applied load are on the next page.


Steel Properties $\mathrm{E}=29,500 \mathrm{ksi}$
$\mathrm{f}_{\mathrm{y}}=33 \mathrm{ksi}$

MASTAN2 does not assume any unit system. Models in MASTAN2 require the use of a consistent set of units. This tutorial will use pound and inch for the model. The later section of the tutorial that determines the internal stresses does include a unit conversion to show stresses in ksi.

## Problem Description - Loading

The pour stop is subjected to a uniform surcharge load, a pressure from the wet concrete, self-weight, and a linear load from similar sources due to interactions with the deck. Uniform distributed loads are available in MASTAN2; however, distributed torsional moments are not possible. To obtain a similar effect the loading will be applied via concentrated point loads and concentrated moments with many smaller elements along the length of the member

## Load Details

See SDI Tech No. 3 for additional information

$$
\begin{aligned}
& \mathrm{p}_{1}=20 \mathrm{psf} \\
& \mathrm{p}_{2}=103.3 \mathrm{psf} \\
& \mathrm{w}_{\mathrm{d}}=0 \text { plf } \downarrow \\
& \text { Resulting Loads } \\
& \mathrm{w}_{\mathrm{y}}=74.0 \mathrm{plf} \downarrow \\
&=6.17 \mathrm{pli} \downarrow \\
& \mathrm{w}_{\mathrm{z}}=35.4 \mathrm{plf} \leftarrow \\
&=2.95 \mathrm{pli} \leftarrow \\
& \mathrm{~m}_{\mathrm{x}}=104.5 \mathrm{in}-\mathrm{lb} / \mathrm{ft} \circlearrowright \\
&=8.71 \mathrm{in}-\mathrm{lb} / \mathrm{in} \circlearrowright
\end{aligned}
$$

## Problem Description - Cross Section

The real pour stop has the rounded geometry shown on the left. The rounded segments, particularly at the top, could be defined by many closely spaced nodes to account for the full radius. However, this tutorial will use the simplified geometry shown on the right based on SDI Tech No. 3.


## Geometry Definition

1) Start with a new, empty model. $\square$
2) From the Geometry menu select Define Node.
3) At the bottom menu bar, click in the edit box to the right of $x=$ and enter 0 . Click in the edit box to the right of $\mathrm{y}=$ and enter 0 . Click in the edit box to the right of $\mathrm{z}=$ and enter 0 .
4) Click on the Apply Button. $\square$
5) From the Geometry menu select Extrude Element.
6) At the bottom menu bar, click on Node 1 to populate the list of nodes. Click in the edit box to the right of Delta $\mathrm{x}=$ and change 0 to 2 .
7) Repeatedly click the $>$ button to the right of Times $=$ to increase 1 to 24 .
8) Click on the Apply Button. $\square$

Clicking the $\square$ icon will advance the tutorial to a page that provides an image of the MASTAN2 interface after the corresponding step is executed. Clicking the $\square$ icon on that page will return you to the step-by-step instructions.



## Cross Section Visualization

1) From the View menu select Defined Views and submenu option Isometric: $x-y-z$.
2) Now with the main member defined, continue to use Extrude Element to illustrate cross section.
3) At the bottom menu bar, click on node 13 to populate the list of nodes. Click in the edit box to the right of Delta $y=$ and change 0 to -1.8405 . Click in the edit box to the right of Delta $z=$ and change 0 to 2.0677.
4) Click on the Apply Button to define an element connecting the centroid to the lower corner of the pour stop cross section which was labeled N2 in the previous cross-section definition. $\square$
5) At the bottom menu bar, click on Node 26 to populate the list of nodes. Click in the edit box to the right of Delta z = and change 0 to -8. Click on the Apply Button. $\square$

Note: If there was another position along the bottom flat where the deflection was of interest, 2 elements could be extruded by altering the process to extrude twice in the $z$ direction with the appropriate Delta $z$ values or by subdividing the bottom element and then moving the new node to the appropriate location.



## Cross Section Visualization Finish

1) Continue defining the cross section by clicking on Node 26 to populate the list of nodes. Click in the edit box to the right of Delta $\mathrm{y}=$ and change 0 to 6.6862. Click on the Apply Button.
2) Click on Node 28 to populate the list of nodes. Click in the edit box to the right of Delta $y=$ and change 0 to 0.2092 . Click in the edit box to the right of Delta $z=$ and change 0 to -0.2092 . Click on the Apply Button.
3) Click on Node 29 to populate the list of nodes. Click in the edit box to the right of Delta $y=$ and change 0 to -0.0613 . Click in the edit box to the right of Delta $z=$ and change 0 to -0.1479 . Click on the Apply Button.
4) Click on Node 30 to populate the list of nodes. Click in the edit box to the right of Delta $y=$ and change 0 to -0.3535 . Click in the edit box to the right of Delta $z=$ and change 0 to -0.3535 . Click on the Apply Button.


Note: For the area where nodes are close together, from the View menu select Zoom Box to be able to zoom in and easier identify which node you are clicking.


## Creating Section Properties

1) From the Properties menu select Define Section.
2) At the bottom menu bar, click on the pop-up menu on the far right that currently displays Basic. Click on Advanced. $\square$
3) Click on MSASect.
4) After the interface loads, click on General to select the radio button next to it. $\square$
5) Click Next to open the editable dialog boxes.
6) Click the edit box to the right of ID: and enter 1. Click the edit box to the right of Z-Coor. $=$ and enter -8. Click the edit box to the right of Y-Coor. = and enter 0. Click Add to save the node. $\square$
7) Repeat entering the values below for each node clicking Add after each one. $\square$

| ID: | 2 | 3 | 4 | 5 | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Z-Coor. $=$ | 0 | 0 | -0.2092 | -0.3571 | -0.7107 |
| Y-Coor. $=$ | 0 | 6.6862 | 6.8954 | 6.8341 | 6.4806 |





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## Creating Section Properties - Cont.

1) Under the segments section, click the edit box to the right of ID: and enter 1. Click the edit box to the right of Start Node= and enter 1. Click the edit box to the right of End Node= and enter 2. Click the edit box to the right of Thickness= and enter 0.1046. Click Add to save the segment. $\square$
2) Repeat entering the values for each segment updating the ID:, Start Node=, and End Node= values by adding 1 to each number until all 5 segments are entered. Click Add after each to save. $\square$
3) Click Calculate to determine the properties. $\square$
4) Click edit box to right of Name: and enter Pour Stop.
5) Click Export to MASTAN2 to copy values to main program. Then click Close to return.

6) Click Apply to save Section 1.


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## Section Properties - Assigning

1) From the Properties menu select Attach Section.
2) At the bottom menu bar, use the buttons to the right of Element(s): to make the list of elements.
3) Create a list of the elements by clicking the All button.
4) Click on the Apply button to assign Section 1. $\square$


## Material Properties

1) From the Properties menu select Define Material.
2) At the bottom menu bar, click in the edit box just to the right of $E=$ and change the 0 to 29500000 (not 29,500,000). Similarly, click in the edit box just to the right of Fy= and change the inf to 33000. Next, click in the edit box to the right of Name: and type Steel. $\square$
3) Click on the Apply button to save Material \#1.
4) From the Properties menu select Attach Material.
5) At the bottom menu bar, create the list of elements to be assigned the properties of Material 1 by clicking on the All button to the right of Elements:. Click on the Apply button.


Since the self-weight is already included in the loading summary, a self-weight was left as zero. If the self-weight was to be included through MASTAN2, a second weightless material would need to be defined and assigned to the members that are being used to visualize the cross section.



## Support Conditions

1) From the Conditions menu select Define Fixities.
2) At the bottom menu bar, define a pin support with torsion fixed support by clicking in the check boxes just to the left of X-disp, Y-disp, Z-disp, and X-rot.
3) Create the list of nodes to be assigned this fixity by clicking on node 1.
4) Click on the Apply button. $\square$
5) At the bottom menu bar, define a roller support with torsion fixed support by clicking in the check boxes just to the left of X-disp to release it and leave Y-disp, Z-disp, and X-rot constrained.
6) Click CIr to empty the list of nodes.
7) Create the list of noes to be assigned this fixity by clicking on node 25.
8) Click on the Apply button. $\square$



## Adding Warping Effects

1) From the Geometry menu select Define Connections and submenu option Torsion.
2) At the bottom menu bar, click on the menu to the right of Warping Restraint for Node $i$ and set the value to Continuous. Repeat this for the Warping Restraint for Node j.
3) Click the Adv button to open pop-up menu. Click the check box next to the $X$-axis option.
4) Create the list of elements to be assigned continuous warping by clicking on the Add button to the advanced menu. Then click on the Apply button. $\square$
5) Click Clr to empty the list of elements. Click on the left most element of the beam.
6) Click on the menu to the right of Warping Restraint for Node i and set the value to Free. Node jis set from the previous step. Click on the Apply button. $\square$
7) Click Clr to empty the list of elements. Click on the right most element of the beam. This might require you to click Adv to close the pop-up menu.
8) Click on the menu to the right of Warping Restraint for Node i and set the value to Continuous. Click on the menu to the right of Warping Restraint for Node j and set the value to Free.
9) Click on the Apply button.



$$
\begin{array}{llll} 
\\
& \\
& \mathrm{N} 16 \\
\mathrm{E} 16
\end{array}
$$

$$
\begin{array}{lll}
\text { E19 } & \text { N20 } \\
& \text { E20 } \\
& \text { N21 } \\
\text { E21 }
\end{array}
$$

Advanced Element Selection




## Loading

1) From the Conditions menu select Define Forces.
2) At the bottom menu bar, click in the edit box just to the right of $P Y=$ and change 0 to -12.34 . Click in the edit box just to the right of $\mathrm{PZ}=$ and change 0 to 5.9.
3) Click the Adv button to open the pop-up menu. To select the main beam nodes, change the edit box to the left of $Z$ to -1 . Change the edit box to the right of $Z$ to 1 .
4) Click Add to add all main beam nodes.
5) Click on the Apply button.

6) From the Conditions menu select Define Moments.
7) At the bottom menu bar, click in the edit box just to the right of $M x=$ and change 0 to -17.42 .
8) Click the Adv button to open the pop-up menu. To select the main beam nodes, change the edit box to the left of $Z$ to -1. Change the edit box to the right of $Z$ to 1.
9) Click Add to add all main beam nodes.
10)Click on the Apply button. $\square$



## Naming and Saving

These steps are technically optional as you can complete analysis without saving or applying a title; however, this is a good time to complete this.

1) From the File menu select Define title. At the bottom menu bar, click in the edit box to the right of Title: and type in a brief description of this effort. This text might include the model title, your name, and/or the assignment number. Click on the Apply button.
2) From the File menu select Save As ... . After selecting your destination folder, type in the filename Pour_Stop and click Save. Note that the top of the window has now changed to include the file name and directory as well as the time the file was last saved.



## First-Order Elastic Analysis

1) From the Analysis menu select Static and submenu option 1st-Order Elastic.
2) At the bottom menu bar, the Analysis Type: should already be set to Space Frame as desired.
3) Click on the Apply button to perform the analysis.

4) From the Results menu select Diagrams and submenu option Deflected Shape.
5) At the bottom menu bar, click on the Apply button.

6) From the Results menu select Node Displacements.
7) On the undeflected shape, click on the midspan node of interest, node 13, and the displacements for base 6 degree of freedoms are provided in the bottom menu bar. $\square$ Results:

| Disp X | Disp Y | Disp Z | Rot X | Rot Y | Rot Z |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\sim 0$ | -0.08033 | -0.0598 | -0.03472 | $\sim 0$ | $\sim 0$ |

8) Clicking on any of the additional nodes representing the cross section will cause the displacements at that location due the combined effects of rotation and translation to be displayed. These deflections do not account for any local axial displacement due to warping though.

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$$


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## Second-Order Elastic Analysis

1) From the Analysis menu select Static and submenu option 2nd-Order Elastic.
2) At the bottom menu bar, the Analysis Type: should already be set to Space Frame as desired.
3) Click on the Apply button to perform the analysis. $\square$
4) From the Results menu select Diagrams and submenu option Deflected Shape.
5) At the bottom menu bar, click on the Apply button. $\square$
6) From the Results menu select Node Displacements.
7) On the undeflected shape, click on the midspan node of interest, node 13, and the displacements for base 6 degree of freedoms are provided in the bottom menu bar. $\square$ Results:

| Disp X | Disp Y | Disp Z | Rot X | Rot Y | Rot Z |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $-2.992 \mathrm{e}-4$ | -0.08758 | -0.06218 | -0.03726 | $\sim 0$ | $\sim 0$ |

The values are similar to the $1^{\text {st-order results but capture the change in the applied torsion that exists }}$ in the deformed condition. The analysis does not account for any change in the direction the load would be applied. The applied loads will remain in the initial orientation.


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| Node: | 13 | Disp X | -0.0002992 | Disp Y | -0.08758 | Disp Z | -0.06218 |  | Status: | Succe | 1.0000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacements |  | Rot X | -0.03726 | Rot $Y$ | -7.556e-09 | Rot Z | -9.059e-09 | (10) 1.000 | $\checkmark$ | Apply | Cancel |

## Section 4: Results and Stresses

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## Using Internal Forces

The next section of this tutorial will provide instructions on how it is possible to calculate the internal stresses from the MASTAN2 output information. After showing how to locate the necessary information from within MASTAN2, the next few pages will provide background and the sign conventions that are used with MASTAN2 to calculate the internal stresses. Some information is provided on how this information can be calculated. Finally, the resulting stresses at midspan are identified using the $2^{\text {nd }}$-order analysis internal forces.

Notes:
The internal forces taken from MASTAN2 are presented with the sign convention shown on the following page. Also included are the required transformations to get to a principal orientation. $\square$
The stress calculations will account for this information.

## Sign Conventions

Node i

$$
\left[\begin{array}{c}
V_{v} \\
V_{w}
\end{array}\right]=\left[\begin{array}{cc}
\cos \phi & \sin \phi \\
-\sin \phi & \cos \phi
\end{array}\right] \cdot\left[\begin{array}{l}
V_{y} \\
V_{z}
\end{array}\right]
$$

Node i


$$
\left[\begin{array}{l}
M_{v} \\
M_{w}
\end{array}\right]=\left[\begin{array}{cc}
\cos \phi & -\sin \phi \\
\sin \phi & \cos \phi
\end{array}\right] \cdot\left[\begin{array}{l}
M_{y} \\
M_{z}
\end{array}\right]
$$

Node i


$$
\left[\begin{array}{c}
v_{s} \\
w_{s}
\end{array}\right]=\left[\begin{array}{cc}
\cos \phi & \sin \phi \\
-\sin \phi & \cos \phi
\end{array}\right] \cdot\left[\begin{array}{l}
y_{s} \\
z_{s}
\end{array}\right]
$$



## Getting Internal Forces

1) From the Results menu select Element Forces.
2) On the undeflected shape, click on the element of interest, element 13, and the internal forces are provided in the bottom menu bar. These are the forces at the start of the member and the middle of the beam. $\square$
3) These forces will be used to calculate the stresses at the middle of the beam.
4) At the bottom menu bar, drag the slider in the left-hand corner until the position indicator located to the right displays 1.00 L .
5) Click on the Apply button. These are the forces at the end of the member. $\square$
6) From this position, the bimoment is required to appropriately divide the longitudinal moment into the standard twisting and warping components for stress calculations.
7) Repeat steps 2 through 5 for element 1 to obtain the end forces to calculate the controlling shear location.
Forces at the start of element $1 \square \quad$ Forces at the end of element $1 \square$




$\xrightarrow[4]{4}$








## Normal Stresses

The internal normal stresses can be calculated in the geometric orientation by

$$
\sigma_{x}=\frac{P}{A}-\frac{\left(M_{y} I_{y z}+M_{z} I_{y y}\right) y+\left(M_{y} I_{z z}+M_{z} I_{y z}\right) z}{I_{y y} I_{z z}-I_{y z}^{2}}+\frac{B \omega_{n}}{C_{\omega}}
$$

This relationship simplifies when working in the principal orientation to

$$
\sigma_{x}=\frac{P}{A}-\frac{M_{w} v}{I_{w w}}-\frac{M_{v} w}{I_{v v}}+\frac{B \omega_{n}}{C_{\omega}}
$$




## Shear Stresses

As part of calculating the shear stresses, the torsional moment must be separated into the component from twisting and the component of warping.

$$
\begin{gathered}
M_{x}-z_{s} V_{y}+y_{s} V_{z}=M_{x}-w_{s} V_{v}+v_{s} V_{w}=T_{T}-T_{\omega} \\
T_{\omega}=\frac{d}{d x} B \approx \frac{\Delta B}{\Delta L}
\end{gathered}
$$

The maximum shear stress is the combination of the stress from transverse shear ( $\tau_{V}$ ), the change in bimoment $\left(\tau_{B}\right)$, and torsion $\left(\tau_{T}\right)$. The transverse and warping terms are approximately uniform across the thickness of the element, whereas torsion linearly varies across the thickness with the extreme value at the surface.

$$
\begin{array}{ll}
\tau_{V}=\frac{\left(-V_{z} I_{y z}+V_{y} I_{y y}\right) \bar{y}+\left(V_{z} I_{z z}-V_{y} I_{y z}\right) \bar{z}}{\left(I_{y y} I_{z z}-I_{y z}^{2}\right) t} A_{s} \\
\tau_{V}=\frac{V_{v} \bar{v}}{I_{w w} t} A_{s}+\frac{V_{w} \bar{w}}{I_{v v} t} A_{s} & \\
\tau_{B}=-\frac{T_{\omega} S_{\omega}}{I_{\omega}} & \tau_{T}=\frac{T_{T} t}{J}
\end{array}
$$

## Calculating Warping Constants

Determining the stresses from warping, both shear stresses and normal stresses, requires the use of warping coefficients. The values can be calculated based on the equations show below with additional details in the following documents. These documents also provide additional information on the stresses calculated as well.
(1) AISC Design Guide 9 (Paul A. Seaburg and Charles J. Carter, 2003)
(2) SDI Technical Note 3. (Steel Deck Institute, 2018)

$$
\begin{aligned}
& \omega_{n s}=\frac{1}{A} \int_{0}^{b} \omega_{o s} t d s-\omega_{o s} \\
& \omega_{o s}=\int_{0}^{s} \rho_{0} d s
\end{aligned}
$$



Different programs exist that can assist in this calculation. One alternative is to make use of CUFSM to calculate these values. The values for the current section are shown here. $\square$


## Resulting Internal Stresses

Each of the items below will link to a stress distribution for the centerline. Note moments and shears below are in the principal orientation.

1) Axial stress from bending moment: $M y$ \& $M z \& A x i a l$ stress from warping: $B \quad \square$
2) Total axial stress from $P, M y, M z, \& B \quad \square$
3) Shear stress from transverse shear: $\mathrm{Vy} \& \mathrm{Vz} \&$ Shear stress from warping: $\mathrm{T}_{\omega} \square$
4) Combined shear stress from $V y, \vee z, \& T_{\omega} \&$ Shear stress from twisting: $T_{T} \square$

No total combined shear stress is shown as the warping and transverse shear stress components are the same across the thickness of the section while the torsional component varies linearly across the thickness of the section with 0 stress at the centerline to $\pm$ the value shown at the extremes.

> Red - Tension, Blue - Compression


## Normal Stresses (ksi) <br> Red - Tension, Blue - Compression



## Shear Stresses (ksi) Red-CCW, Blue - CW



Results do not account for increase that could be considered in shear forces and torsion since part of the end point loads would be on this member.

## Shear Stresses (ksi) Red-CCW, Blue - CW




Results do not account for increase that could be considered in shear forces and torsion since part of the end point loads would be on this member.

## Section 5: Additional Options

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## Other Possibilities

MASTAN2 has many options of what can be done. For this tutorial, three ideas are presented. Each possibility is completed starting with the initial model completed to this point. To compare to each of the following, it is recommended to make sure you have a base version of this model saved to be able to start over.

1) Applying uniform loading instead of point loads for the lateral loading.
2) Adjusting the boundary conditions to consider the effects of fixed warping.
3) Updating the model to calculate the results for other lengths or check other critical geometry.

## 1) Uniform Loading

While a distributed moment loading is not currently available in MASTAN2, it would be possible to use a distributed uniform load instead of point loads using the steps below.

1) From the Conditions menu select Define Forces.
2) At the bottom menu bar, all loads should be 0 .
3) Click the All button to populate the list of nodes.
4) Click on the Apply button to remove all point loads. $\square$
5) From the Conditions menu select Define Uniform Loads.
6) At the bottom menu bar, click on Element(s) local $x^{\prime}-y^{\prime}-z^{\prime}$ to open the drop-down menu. Select System global X-Y-Z.
7) Click in the edit box just to the right of $\mathrm{Wy}=$ and change 0 to -6.17. Click in the edit box just to the right of $\mathrm{Wz}=$ and change 0 to -2.95. Click the Adv button to open pop-up menu. Ensure the check box next to the X -axis option is selected.
8) Click Add to add the main beam elements to the element list.
9) Click on the Apply button. $\square$

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## 1) Uniform Loading -- Second-Order Elastic Analysis

1) From the Analysis menu select Static and submenu option 2nd-Order Elastic.
2) At the bottom menu bar, the Analysis Type: should already be set to Space Frame as desired.
3) Click on the Apply button to perform the analysis.
4) From the Results menu select Node Displacements.
5) On the undeflected shape, click on the midspan node of interest, node 13 , and the displacements for base 6 degree of freedoms are provided in the bottom menu bar. $\square$

Results:

| Disp X | Disp Y | Disp Z | Rot X | Rot $Y$ | Rot Z |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $-2.992 \mathrm{e}-4$ | -0.08758 | -0.06217 | -0.03726 | $\sim 0$ | $\sim 0$ |

The values are similar to using point loads as the model was meshed adequately. If one would be working with less elements with a longer length, a greater variation would be expected with bending moment. There is not an effect of distributed torsion included.


| Node: | 13 |
| :---: | ---: |
| Displacements |  |


-0.0002992
Displacements
Disp
Rot Y
Rot X
Rot $Z$
$-9.063 \mathrm{e}-09$
Appl
$4 \equiv$

## 2) Alternate Boundary Conditions

The use of MASTAN2 allows for different boundary conditions. While the model does not need to have symmetric supports, for a reference solution the ends were left as pin supports with torsion fixed while the warping constraint was changed to fixed.

1) From the Geometry menu select Define Connections and submenu option Torsion.
2) Click on the left most element of the beam.
3) At the bottom menu bar, click on the menu to the right of Warping Restraint for Node i and set the value to Fixed. Click on the menu to the right of Warping Restraint for Node $j$ and set the value to Continuous.
4) Click on the Apply button.

5) Click CIr to empty the list of elements. Click on the right most element of the beam. This might require you to click Adv to close the pop-up menu.
6) Click on the menu to the right of Warping Restraint for Node i and set the value to Continuous. Click on the menu to the right of Warping Restraint for Node jand set the value to Fixed.
7) Click on the Apply button.




## 2) Alternate Boundary Conditions -- $2^{\text {nd }}-O r d e r$ Elastic Analysis

1) From the Analysis menu select Static and submenu option 2nd-Order Elastic.
2) At the bottom menu bar, the Analysis Type: should already be set to Space Frame as desired.
3) Click on the Apply button to perform the analysis.
4) From the Results menu select Node Displacements.
5) Click on the midspan node of interest, node 13, and the displacements for base 6 degree of freedoms are provided in the bottom menu bar. $\square$

Results:

| Disp X | Disp Y | Disp Z | Rot X | Rot Y | Rot Z |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $-2.684 \mathrm{e}-5$ | -0.02776 | -0.01727 | -0.01106 | $\sim 0$ | $\sim 0$ |

6) From the Results menu select Element Forces.
7) On the undeflected shape, click on the element of interest, element 13 , and the internal forces are provided in the bottom menu bar. These are the forces at the start of the member and the middle of the beam. $\square$



## 3) Updating the Geometry -- Scaling

A newer feature of MASTAN2 allows for the length of the model to quickly updated.

1) From the Geometry menu select Scale Node(s).
2) At the bottom menu bar, click in the edit box to the right of $C x=$ and change 1 to 0.5 . This will scale the model only in the $x$-direction making the overall length of the beam 24 inches.
3) Click the All button to populate the list of nodes.
4) Click on the Apply button. $\square$


Define node(s) and scaling input
O About point coords:
Scale factors
caling input
$x=$
$C x=$

| Node(s): |
| :---: |
| 0 | $y=$

$C y=$

| All | Clr | Adv |
| :--- | :--- | :--- |

Status:
0.5

## 3) Updating the Geometry - Update Loading

1) From the Conditions menu select Define Forces.
2) At the bottom menu bar, click in the edit box just to the right of $P Y=$ and change 0 to -6.17 . Click in the edit box just to the right of $\mathrm{PZ}=$ and change 0 to 2.95 .
3) Click the Adv button to open the pop-up menu. To select the main beam nodes, change the edit box to the left of $Z$ to -1. Change the edit box to the right of $Z$ to 1 .
4) Click Add to add all main beam nodes.
5) Click on the Apply button.

6) From the Conditions menu select Define Moments.
7) At the bottom menu bar, click in the edit box just to the right of $M x=$ and change 0 to -8.71 .
8) Click the Adv button to open the pop-up menu. To select the main beam nodes, change the edit box to the left of $Z$ to -1. Change the edit box to the right of $Z$ to 1 .
9) Click Add to add all main beam nodes.
10)Click on the Apply button. $\square$



## 3) Updating the Geometry -- $2^{\text {nd }}$-Order Elastic Analysis

1) From the Analysis menu select Static and submenu option 2nd-Order Elastic.
2) At the bottom menu bar, the Analysis Type: should already be set to Space Frame as desired.
3) Click on the Apply button to perform the analysis.
4) From the Results menu select Node Displacements.
5) Click on the midspan node of interest, node 13, and the displacements for base 6 degree of freedoms are provided in the bottom menu bar. $\square$
Results:

| Disp X | Disp Y | Disp Z | Rot X | Rot $Y$ | Rot Z |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $-4.818 \mathrm{e}-6$ | -0.007676 | -0.005841 | $-3.356 \mathrm{e}-3$ | $\sim 0$ | $\sim 0$ |

6) From the Results menu select Element Forces.
7) On the undeflected shape, click on the element of interest, element 13 , and the internal forces are provided in the bottom menu bar. These are the forces at the start of the member and the middle of the beam. $\square$


| Node: | 13 | Disp X | -4.818e-06 | Disp Y | -0.007676 | Disp Z | -0.005841 |  | Status: | Succes | 1.0000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacements |  | Rot X | -0.003356 | Rot $Y$ | -1.092e-11 | Rot Z | -1.236e-11 | (10) 1.000 | $\checkmark$ | Apply | Cancel |



## 3) Updating the Geometry -- Additional Sections

If other critical locations for the displacement of the cross section are needed, we can duplicate the existing cross section that was modeled.

1) From the Geometry menu select Duplicate Element(s).
2) At the bottom menu bar, click in the edit box to the right of Delta $x=$ and change 0 to -2. Ensure the check box next to Include Attributes is selected to include the property information is included.
3) Click the Adv button to open the pop-up menu. Ensure the check box next to $X$-axis is selected.
4) To select the illustrated cross section, click All next to the Element(s): window. Then click the Remove button.
5) Repeatedly click the $>$ button to the right of Times $=$ to increase 1 to 5 .
6) Click on the Apply button. $\square$

The analysis is not run again as the addition of these elements will not change the results. It would just provide more information on the displacement of the cross section.



## This completes the tutorial.

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